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COMPARISON OF WIND INPUT DATA FOR USE  
IN DETERMINATION OF MISSILE AND SPACE  
VEHICLE DESIGN BY STATISTICAL METHODS

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DYNAMICS ANALYSIS BRANCH  
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## ABSTRACT

This report presents a comparison of selected statistical wind summaries compiled from upper air observations made at Patrick AFB, Florida. A description of how this data was developed into covariance matrices is presented. Also a brief outline of how these covariance matrices can be utilized in control and trajectory studies is considered.

## ACKNOWLEDGMENT

The authors of this report gratefully acknowledge the assistance of Mr. D. H. Boen in the many computations required in a report of this type. The assistance of Mr. Sieja in developing a program for calculating the covariance matrices on the Burroughs 205 Computer is also acknowledged.

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## I. INTRODUCTION

The ultimate objective in designing a missile or space vehicle would be to consider the simultaneous effects of its entire flight environment. This flight environment is composed of pressure, temperature, density, and winds usually random in nature, which may be described in a statistical form. The process for describing this environment should be nonstationary rather than the standard stationary method. Stationary random processes are characterized by a set of probability functions that are invariant with a change in the time origin. When variations with time take place, the process is said to be non-stationary. Since the missile or space vehicle changes altitude as a function of time, the wind velocity for any time varies as a function of both altitude and time. Therefore, non-stationary random processes should be used to properly describe the environment.

Previous efforts have considered the effects of wind velocities separately from wind gusts or turbulence. R. E. Bieber (see reference one) proposed a method which utilized non-stationary statistical methods to determine missile structural loads. He demonstrated how the effects of wind velocity combined with turbulence or gusts might be studied simultaneously. The purpose of this report is to compare the data that Mr. Bieber utilized for a one dimensional input with the data supplied by the Aerophysics and Geophysics Branch. This branch is preparing the required cross-correlation coefficients in order to complete the two dimensional wind input data. Work is also underway preparing the means, standard deviations, and correlation coefficients for atmospheric density at various geographical locations.

## II. DEVELOPMENT OF THE COVARIANCE MATRIX FROM THE CORRELATION COEFFICIENTS AND STANDARD DEVIATIONS

The Geophysics and Aerophysics Branch of the Aeroballistics Laboratory supplied the data shown in Tables 2 and 3. The procedure followed in developing the wind covariance matrix is shown in Figure 1. The standard deviation at one altitude for the North-South (meridional) wind is multiplied by the standard deviation at another altitude and this product is then multiplied by the correlation coefficient relating these different North-South winds. This computation is repeated until all the values of the North-South covariance matrix are obtained. The same procedure is then repeated for the East-West zonal winds covariance matrix.

The North-South wind covariance is then added to the East-West wind covariance to form a combined matrix. To the diagonal terms of this combined matrix is added the diagonal terms of the North-South to the East-West covariance matrix and the diagonal terms of East-West to the North-South covariance matrix. The resultant matrix represents an incomplete two dimensional matrix. This matrix was utilized as a one dimensional input by Mr. R. E. Bieber (reference one). The resulting incomplete two dimensional matrix is symmetrical, consequently only a triangular matrix need be shown. The two dimensional matrix can be completely developed by utilizing the non-diagonal parts of the North-South with East-West and the East-West with the North-South covariance matrices.

### III. DESCRIPTION AND COMPARISON OF THE COVARIANCE MATRICES PRESENTED IN THIS REPORT

The statistical procedures employed to develop the covariance matrices shown in Tables 4, 5, and 6 were identical. The basic data used to develop the covariance matrices were obtained from the correlation matrices shown in Tables 1, 2, and 3. The conversion of the correlation coefficients, and the standard deviations to the covariance matrices was accomplished by utilizing the following formula. (Where X and Y are random variables)

$$\text{COVARIANCE (XY)} = \left[ \begin{array}{c} \text{CORRELATION (XY)} \\ \text{COEFFICIENT} \end{array} \right] \left[ \begin{array}{c} \text{STANDARD (X)} \\ \text{DEVIATION} \end{array} \right] \left[ \begin{array}{c} \text{STANDARD (Y)} \\ \text{DEVIATION} \end{array} \right]$$

The main purpose of this report is to compare Mr. Bieber's covariances with those developed by the Aeroballistics Laboratory. Although the same procedures were employed in the computation of these matrices (Tables 4, 5, and 6), there exists differences in the results obtained. Tables 7, 8, 9, and 10 provides a comparison of Bieber's data with the Aeroballistics Laboratory Data. The values shown in Table 2 were subtracted from the values shown in Table 1, to form Table 7. The values shown in Table 3 were subtracted from the values shown in Table 1 to form Table 8. The values shown in Table 5 were subtracted from the values shown in Table 4 to form Table 9. The values shown in Table 6 were subtracted from the values shown in Table 4 to form Table 10. The differences in the covariance matrices due to the different arrangements (reference period and period of record) of the basic observation data.

The basic data used in the computations are:

- (1) Table 4 employed wind data for the winter months (December, January, February) observed during the period Feb. 1950 thru Feb. 1955.
- (2) Table 5 employed wind data only for the month of January as observed from January 1951 - December 1957.
- (3) Table 6 employed all wind data observed during the period January 1951 thru December 1957.

Therefore, the difference between Table 4 and Tables 5 and 6 result partially from combining the observational data on a monthly, seasonal, or annual basis. It may be seen from this presentation that a seasonal (winter) covariance matrix (Table 4) results in moderate conditions relative to the monthly (January) covariance matrix. Table 5 combines the upper air wind data for a winter month (January) only and, in general, has the highest values for the covariance matrix. Due to the influence of the summer months the annual covariance has the lower covariance values. This report, therefore, illustrates the relative differences in wind data statistically grouped according to different time reference periods. The selection of which covariance matrix to use depends upon the objective of the investigation and detail on wind input data desired.

### IV. UTILIZATION OF THE COVARIANCE MATRIX IN CONTROL AND TRAJECTORY STUDIES

There are several ways in which the covariance matrix might be utilized in order to obtain a statistical description of the system response to winds

and/or turbulence. The approach that seems to be the most efficient consists of taking the square root of the covariance matrix.

Figure 2 shows the flow of information when the square root of the covariance matrix method is used to develop a statistical description of the system parameters. Starting with the covariance matrix, the eigenvalues and eigenvectors are determined by using conventional techniques. For every eigenvalue there is a set of eigenvectors, consequently as the size of the covariance matrix increases the amount of work to solve for the eigenvalues and eigenvectors increases. The eigenvector matrix multiplied by the square root of the eigenvalue diagonal matrix is then multiplied by the transpose of the eigenvector matrix. The resultant matrix is the square root of the covariance matrix.

The columns for the square root of the covariance matrix are then fed into the computer program as discrete profiles. The response of the system parameters to each one of these discrete profiles represents a column of the (parameter response) matrix. When all of the profiles have been run by the computer the matrix can be completely assembled. This matrix is then multiplied by its transpose. The resulting matrix represents the response to the covariance matrix for all the system parameters. The square root of the diagonal terms of this matrix represents the standard deviation from the mean for each parameter as a function of altitude. The standard deviation from the mean is multiplied by the desired number of sigmas and then added to the response to the mean value for the winds. The resultant functions of altitude represent statistical description of the control system responses.

Structural bending is a function of the output parameters of the trajectory. Therefore, it is a straightforward matter to utilize these parameter values to determine actual structural loads.



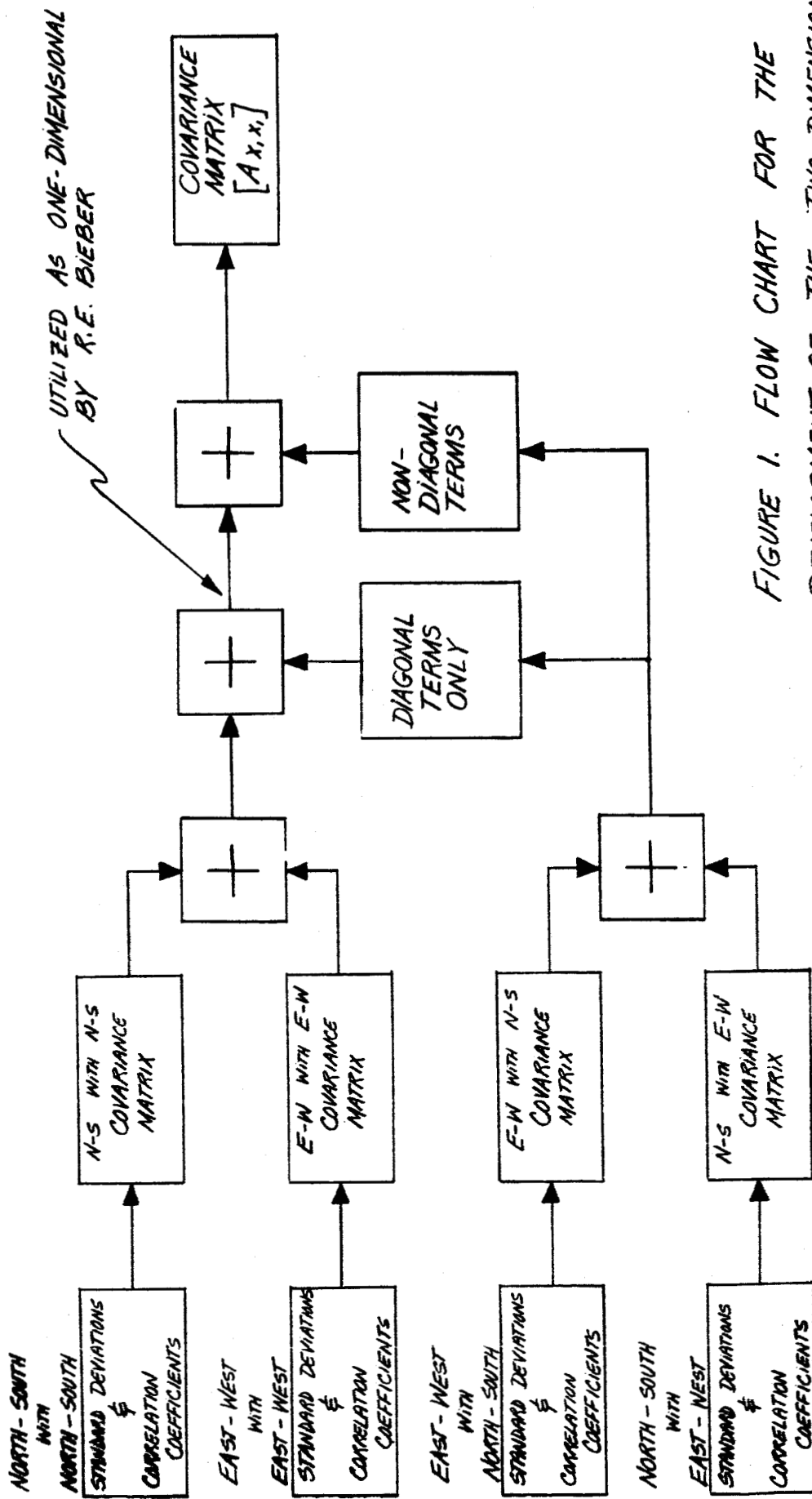
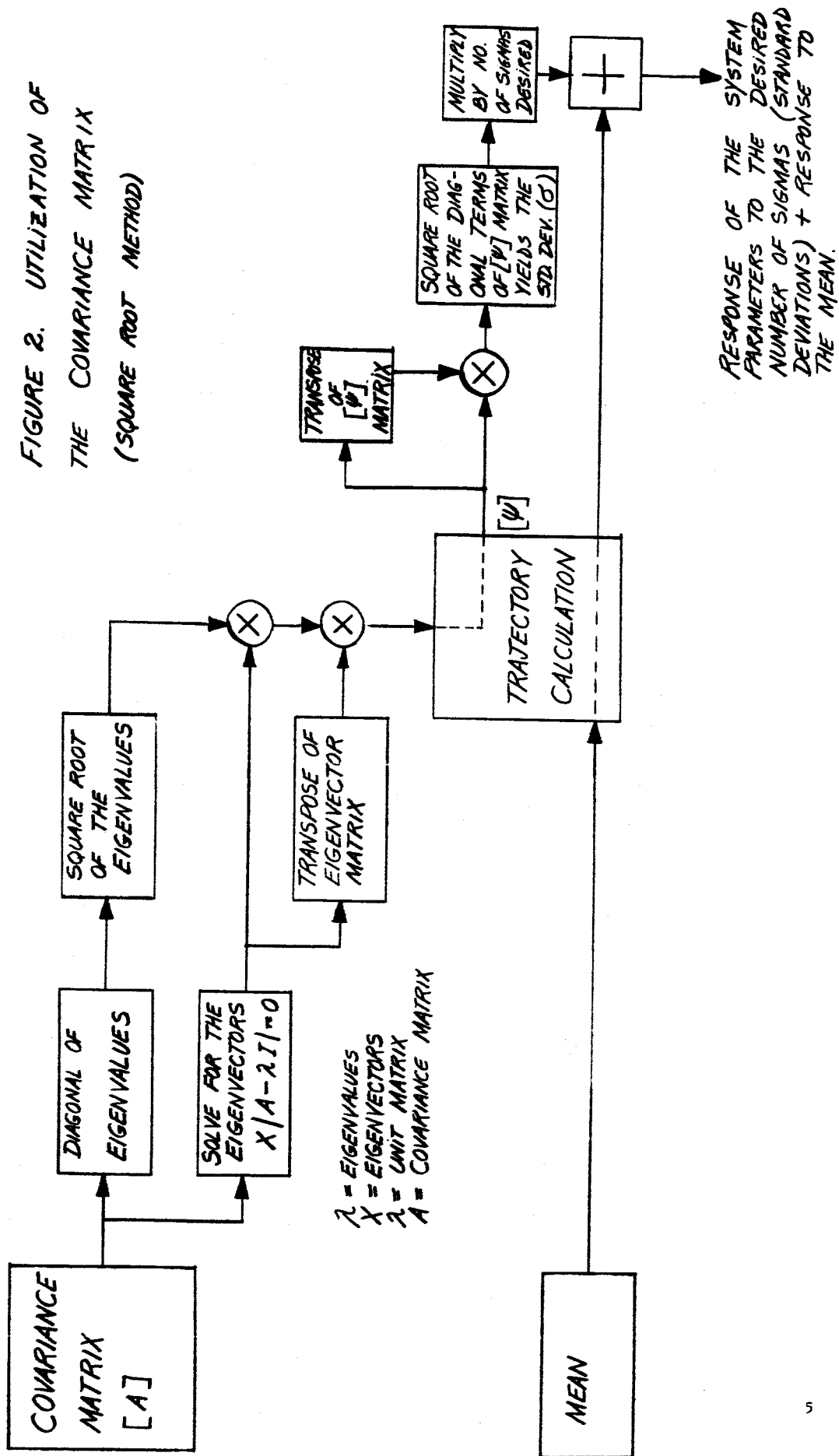


FIGURE 1. FLOW CHART FOR THE  
DEVELOPMENT OF THE TWO-DIMENSIONAL  
WIND COVARIANCE.



NOTE: Zonal Mean, Positive for Wind Component from West; Meridional Mean, Positive for Wind Component from South. Underlined Values Indicate Intraseasonal Correlations

TABLE 2.  
INTERLEVEL AND INTRALEVEL CORRELATIONS BETWEEN WIND SPEED COMPONENTS WITH MEANS AND STANDARD DEVIATIONS BY ALTITUDE LEVELS

STATION		STATION ELEVATION		STATION COORDINATES		PERIOD OF OBSERVATION		DATA SOURCE		PREPARED BY		PATRICK AFB, FLORIDA CAPE CANAVERAL, FLORIDA	
Patrick AFB 7 meters MSL Cape Canaveral 5 meters MSL		Patrick AFB 28 deg 14 min N, 80 deg 36 min W Cape Canaveral 28 deg 25 min N, 80 deg 33 min W		Patrick AFB January 1951-17 November 1954 Cape Canaveral 18 November 1950-December 1957		National Weather Records Center U. S. Weather Bureau Arlington, North Carolina		Army Ballistic Missile Agency Aeroballistics Laboratory Redstone Arsenal, Alabama 23 February 1960				JANUARY	
REFERENCE PERIOD		Altitude (MSL) km		Mean MSL m/s		Mean MSL m/s		Mean MSL m/s		Mean MSL m/s		Mean MSL m/s	
No.	Altitude (MSL) km	Mean MSL m/s	Mean MSL m/s	Mean MSL m/s	Mean MSL m/s	Mean MSL m/s	Mean MSL m/s	Mean MSL m/s	Mean MSL m/s	Mean MSL m/s	Mean MSL m/s	Mean MSL m/s	Mean MSL m/s
419	0.76	3.95	3.95	3.95	3.95	3.95	3.95	3.95	3.95	3.95	3.95	3.95	3.95
406	1	7.33	7.33	7.33	7.33	7.33	7.33	7.33	7.33	7.33	7.33	7.33	7.33
410	2	9.46	9.46	9.46	9.46	9.46	9.46	9.46	9.46	9.46	9.46	9.46	9.46
413	3	8.64	8.64	8.64	8.64	8.64	8.64	8.64	8.64	8.64	8.64	8.64	8.64
413	4	12.00	12.00	12.00	12.00	12.00	12.00	12.00	12.00	12.00	12.00	12.00	12.00
413	5	18.28	18.28	18.28	18.28	18.28	18.28	18.28	18.28	18.28	18.28	18.28	18.28
411	6	18.08	18.08	18.08	18.08	18.08	18.08	18.08	18.08	18.08	18.08	18.08	18.08
409	7	21.05	21.05	21.05	21.05	21.05	21.05	21.05	21.05	21.05	21.05	21.05	21.05
407	8	24.22	24.22	24.22	24.22	24.22	24.22	24.22	24.22	24.22	24.22	24.22	24.22
403	9	26.76	26.76	26.76	26.76	26.76	26.76	26.76	26.76	26.76	26.76	26.76	26.76
397	10	30.07	30.07	30.07	30.07	30.07	30.07	30.07	30.07	30.07	30.07	30.07	30.07
389	11	32.82	32.82	32.82	32.82	32.82	32.82	32.82	32.82	32.82	32.82	32.82	32.82
380	12	34.50	34.50	34.50	34.50	34.50	34.50	34.50	34.50	34.50	34.50	34.50	34.50
389	13	34.45	34.45	34.45	34.45	34.45	34.45	34.45	34.45	34.45	34.45	34.45	34.45
332	14	35.51	35.51	35.51	35.51	35.51	35.51	35.51	35.51	35.51	35.51	35.51	35.51
302	18	30.56	30.56	30.56	30.56	30.56	30.56	30.56	30.56	30.56	30.56	30.56	30.56
286	16	25.87	25.87	25.87	25.87	25.87	25.87	25.87	25.87	25.87	25.87	25.87	25.87
227	17	20.82	20.82	20.82	20.82	20.82	20.82	20.82	20.82	20.82	20.82	20.82	20.82
209	18	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30	14.30
194	19	10.25	10.25	10.25	10.25	10.25	10.25	10.25	10.25	10.25	10.25	10.25	10.25
182	20	6.63	6.63	6.63	6.63	6.63	6.63	6.63	6.63	6.63	6.63	6.63	6.63
172	21	4.07	4.07	4.07	4.07	4.07	4.07	4.07	4.07	4.07	4.07	4.07	4.07
162	22	3.23	3.23	3.23	3.23	3.23	3.23	3.23	3.23	3.23	3.23	3.23	3.23
150	23	2.79	2.79	2.79	2.79	2.79	2.79	2.79	2.79	2.79	2.79	2.79	2.79
138	24	3.53	3.53	3.53	3.53	3.53	3.53	3.53	3.53	3.53	3.53	3.53	3.53
128	25	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94	4.94
112	26	5.80	5.80	5.80	5.80	5.80	5.80	5.80	5.80	5.80	5.80	5.80	5.80
89	27	5.92	5.92	5.92	5.92	5.92	5.92	5.92	5.92	5.92	5.92	5.92	5.92
71	28	5.54	5.54	5.54	5.54	5.54	5.54	5.54	5.54	5.54	5.54	5.54	5.54
57	29	7.07	7.07	7.07	7.07	7.07	7.07	7.07	7.07	7.07	7.07	7.07	7.07
44	30	9.63	9.63	9.63	9.63	9.63	9.63	9.63	9.63	9.63	9.63	9.63	9.63
30	31	11.85	11.85	11.85	11.85	11.85	11.85	11.85	11.85	11.85	11.85	11.85	11.85
34	32	13.21	13.21	13.21	13.21	13.21	13.21	13.21	13.21	13.21	13.21	13.21	13.21

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TABLE 3:  
INTERLEVEL AND INTRALEVEL CORRELATIONS BETWEEN WIND SPEED COMPONENTS WITH MEANS AND STANDARD DEVIATIONS OF WIND SPEED COMPONENTS BY ALTITUDE LEVELS

STATION	STATION ELEVATION	STATION COORDINATES	PERIOD OF OBSERVATION	DATA SOURCE	PREPARED BY	PATRICK AFB, FLORIDA CAPE CANAVERAL, FLORIDA																														
						ANNUAL																														
No. of (MILES)	Altitude (MILES)	Altitude (MILES)	REFERENCE PERIOD																																	
			1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31			
4844	1.06	0.48	0.51	0.36	0.13	-0.08	-0.27	-0.46	0.37	-0.78	-1.08	-1.30	-1.88	-2.01	-1.68	-1.36	-0.93	-0.61	-0.38	-0.11	0.07	0.19	0.33	0.15	0.15	0.18	0.24	0.36	0.48	0.70	1.54					
4845	3.72	5.31	5.30	5.71	6.31	6.85	7.42	8.48	9.40	10.53	11.99	13.22	13.47	12.78	11.28	9.24	7.08	5.72	5.47	4.38	3.94	3.85	3.73	3.42	3.68	3.79	4.24	4.49	4.95	5.43	5.87					
4846	-0.17	4.54	4.53	5.40	5.84	6.25	6.64	7.02	7.39	7.75	8.11	8.47	8.83	9.19	9.55	9.91	10.27	10.63	10.99	11.35	11.71	12.07	12.43	12.79	13.15	13.51	13.87	14.23	14.59	14.95	15.31					
4847	6.90	0.67	0.61	0.51	0.47	0.37	0.25	0.10	0.12	0.02	-0.04	-0.06	-0.13	-0.13	-0.03	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04	-0.04					
4848	6.16	3.30	0.93	0.05	0.42	0.93	1.41	1.89	2.36	2.82	3.28	3.74	4.20	4.66	5.12	5.58	6.04	6.50	6.96	7.42	7.88	8.34	8.80	9.26	9.72	10.18	10.64	11.10	11.56	12.02	12.48					
4849	5.95	7.06	8.00	8.92	9.84	10.76	11.68	12.60	13.52	14.44	15.36	16.28	17.20	18.12	19.04	19.96	20.88	21.80	22.72	23.64	24.56	25.48	26.40	27.32	28.24	29.16	30.08	31.00	31.92	32.84	33.76					
4850	5.04	6.17	7.31	8.48	9.65	10.82	11.99	13.16	14.33	15.50	16.67	17.84	19.01	20.18	21.35	22.52	23.69	24.86	26.03	27.20	28.37	29.54	30.71	31.88	33.05	34.22	35.39	36.56	37.73	38.90	40.07					
4851	4.82	5.48	6.25	7.02	7.79	8.56	9.33	10.10	10.87	11.64	12.41	13.18	13.95	14.72	15.49	16.26	17.03	17.80	18.57	19.34	20.11	20.88	21.65	22.42	23.19	23.96	24.73	25.50	26.27	27.04	27.81					
4852	4.08	4.44	4.78	5.08	5.38	5.68	5.98	6.28	6.58	6.88	7.18	7.48	7.78	8.08	8.38	8.68	8.98	9.28	9.58	9.88	10.18	10.48	10.78	11.08	11.38	11.68	11.98	12.28	12.58	12.88	13.18					
4853	3.72	4.05	4.31	4.54	4.76	4.98	5.20	5.42	5.64	5.86	6.08	6.30	6.52	6.74	6.96	7.18	7.40	7.62	7.84	8.06	8.28	8.50	8.72	8.94	9.16	9.38	9.60	9.82	10.04	10.26	10.48					
4854	3.34	3.80	4.25	4.69	5.13	5.57	6.01	6.45	6.89	7.33	7.77	8.21	8.65	9.09	9.53	9.97	10.41	10.85	11.29	11.73	12.17	12.61	13.05	13.49	13.93	14.37	14.81	15.25	15.69	16.13	16.57					
4855	3.09	3.50	3.90	4.30	4.70	5.10	5.50	5.90	6.30	6.70	7.10	7.50	7.90	8.30	8.70	9.10	9.50	9.90	10.30	10.70	11.10	11.50	11.90	12.30	12.70	13.10	13.50	13.90	14.30	14.70	15.10					
4856	2.85	3.25	3.65	4.05	4.45	4.85	5.25	5.65	6.05	6.45	6.85	7.25	7.65	8.05	8.45	8.85	9.25	9.65	10.05	10.45	10.85	11.25	11.65	12.05	12.45	12.85	13.25	13.65	14.05	14.45	14.85					
4857	2.61	3.01	3.41	3.81	4.21	4.61	5.01	5.41	5.81	6.21	6.61	7.01	7.41	7.81	8.21	8.61	9.01	9.41	9.81	10.21	10.61	11.01	11.41	11.81	12.21	12.61	13.01	13.41	13.81	14.21	14.61					
4858	2.37	2.77	3.17	3.57	3.97	4.37	4.77	5.17	5.57	5.97	6.37	6.77	7.17	7.57	7.97	8.37	8.77	9.17	9.57	9.97	10.37	10.77	11.17	11.57	11.97	12.37	12.77	13.17	13.57	13.97	14.37					
4859	2.13	2.53	2.93	3.33	3.73	4.13	4.53	4.93	5.33	5.73	6.13	6.53	6.93	7.33	7.73	8.13	8.53	8.93	9.33	9.73	10.13	10.53	10.93	11.33	11.73	12.13	12.53	12.93	13.33	13.73	14.13					
4860	1.89	2.29	2.69	3.09	3.49	3.89	4.29	4.69	5.09	5.49	5.89	6.29	6.69	7.09	7.49	7.89	8.29	8.69	9.09	9.49	9.89	10.29	10.69	11.09	11.49	11.89	12.29	12.69	13.09	13.49	13.89					
4861	1.65	2.05	2.45	2.85	3.25	3.65	4.05	4.45	4.85	5.25	5.65	6.05	6.45	6.85	7.25	7.65	8.05	8.45	8.85	9.25	9.65	10.05	10.45	10.85	11.25	11.65	12.05	12.45	12.85	13.25	13.65					
4862	1.41	1.81	2.21	2.61	3.01	3.41	3.81	4.21	4.61	5.01	5.41	5.81	6.21	6.61	7.01	7.41	7.81	8.21	8.61	9.01	9.41	9.81	10.21	10.61	11.01	11.41	11.81	12.21	12.61	13.01	13.41					
4863	1.17	1.57	1.97	2.37	2.77	3.17	3.57	3.97	4.37	4.77	5.17	5.57	5.97	6.37	6.77	7.17	7.57	7.97	8.37	8.77	9.17	9.57	9.97	10.37	10.77	11.17	11.57	11.97	12.37	12.77	13.17					
4864	0.93	1.33	1.73	2.13	2.53	2.93	3.33	3.73	4.13	4.53	4.93	5.33	5.73	6.13	6.53	6.93	7.33	7.73	8.13	8.53	8.93	9.33	9.73	10.13	10.53	10.93	11.33	11.73	12.13	12.53	12.93					
4865	0.69	1.09	1.49	1.89	2.29	2.69	3.09	3.49	3.89	4.29	4.69	5.09	5.49	5.89	6.29	6.69	7.09	7.49	7.89	8.29	8.69	9.09	9.49	9.89	10.29	10.69	11.09	11.49	11.89	12.29	12.69					
4866	0.45	0.85	1.25	1.65	2.05	2.45	2.85	3.25	3.65	4.05	4.45	4.85	5.25	5.65	6.05	6.45	6.85	7.25	7.65	8.05	8.45	8.85	9.25	9.65	10.05	10.45	10.85	11.25	11.65	12.05	12.45					
4867	0.21	0.61	1.01	1.41	1.81	2.21	2.61	3.01	3.41	3.81	4.21	4.61	5.01	5.41	5.81	6.21	6.61	7.01	7.41	7.81	8.21	8.61	9.01	9.41	9.81	10.21	10.61	11.01	11.41	11.81	12.21					
4868	-0.03	0.37	0.77	1.17	1.57	1.97	2.37	2.77	3.17	3.57	3.97	4.37	4.77	5.17	5.57	5.97	6.37	6.77	7.17	7.57	7.97	8.37	8.77	9.17	9.57	9.97	10.37	10.77	11.17	11.57	11.97					
4869	-0.29	0.11	0.51	0.91	1.31	1.71	2.11	2.51	2.91	3.31	3.71	4.11	4.51	4.91	5.31	5.71	6.11	6.51	6.91	7.31	7.71	8.11	8.51	8.91	9.31	9.71	10.11	10.51	10.91	11.31	11.71					
4870	-0.55	-0.15	0.25	0.65	1.05	1.45	1.85	2.25	2.65	3.05	3.45	3.85	4.25	4.65	5.05	5.45	5.85	6.25	6.65	7.05	7.45	7.85	8.25	8.65	9.05	9.45	9.85	10.25	10.65	11.05	11.45					
4871	-0.81	-0.41	0.01	0.41	0.81	1.21	1.61	2.01	2.41	2.81	3.21	3.61	4.01	4.41	4.81	5.21	5.61	6.01	6.41	6.81	7.21	7.61	8.01	8.41	8.81	9.21	9.61	10.01	10.41	10.81	11.21					
4872	-1.07	-0.67	-0.27	0.13	0.53	0.93	1.33	1.73	2.13	2.53	2.93	3.33	3.73	4.13	4.53	4.93	5.33	5.73	6.13	6.53	6.93	7.33	7.73	8.13	8.53	8.93	9.33	9.73	10.13	10.53	10.93					
4873	-1.33	-0.93	-0.53	-0.13	0.27	0.67	1.07	1.47	1.87	2.27	2.67	3.07	3.47	3.87	4.27	4.67	5.07	5.47	5.87	6.27	6.67	7.07	7.47	7.87	8.27	8.67	9.07	9.47	9.87	10.27	10.67					
4874	-1.59	-1.19	-0.79	-0.39	0.01	0.41	0.81	1.21	1.61	2.01	2.41	2.81	3.21	3.61	4.01	4.41	4.81	5.21	5.61	6.01	6.41	6.81	7.21	7.61	8.01	8.41	8.81	9.21	9.61	10.01	10.41					
4875	-1.85	-1.45	-1.05	-0.65	-0.25	0.15	0.55	0.95	1.35	1.75	2.15	2.55	2.95	3.35	3.75	4.15	4.55	4.95	5.35	5.75	6.15	6.55	6.95	7.35	7.75	8.15	8.55	8.95	9.35	9.75	10.15					
4876	-2.11	-1.71	-1.31	-0.91	-0.51	-0.11	0.29	0.69	1.09	1.49	1.89	2.29	2.69	3.09	3.49	3.89	4.29	4.69	5.09	5.49	5.89	6.29	6.69	7.09	7.49	7.89	8.29	8.69	9.09	9.49	9.89					
4877	-2.37	-1.97	-1.57	-1.17	-0.77	-0.37	0.03	0.43	0.83	1.23	1.63	2.03	2.43	2.83	3.23	3.63	4.03	4.43	4.83	5.23	5.63	6.03	6.43	6.83	7.23	7.63	8.03	8.43	8.83	9.23	9.63					
4878	-2.63	-2.23	-1.83	-1.43	-1.03	-0.63	-0.23	0.17	0.57	0.97	1.37	1.77	2.17	2.57	2.97	3.37	3.77	4.17	4.57	4.97	5.37	5.77	6.17	6.57	6.97	7.37	7.77	8.17	8.57	8.97	9.37					
4879	-2.89	-2.49	-2.09	-1.69	-1.29	-0.89	-0.49	0.11	0.51	0.91	1.31	1.71	2.11	2.51	2.91	3.31	3.71	4.11	4.51	4.91	5.31	5.71	6.11	6.51	6.91	7.31	7.71	8.11	8.51	8.91	9.31					
4880	-3.15	-2.75	-2.35	-1.95	-1.55	-1.15	-0.75	0.05	0.45	0.85	1.25	1.65	2.05	2.45	2.85	3.25	3.65	4.05	4.45	4.85	5.25	5.65	6.05	6.45	6.85	7.25	7.65	8.05	8.45	8.85	9.25					
4881	-3.41	-3.01	-2.61	-2.21	-1.81	-1.41	-1.01	0.39	0.79	1.19	1.59	1.99	2.39	2.79	3.19	3.59	3.99	4.39	4.79	5.19	5.59	5.99	6.39	6.79	7.19	7.59	7.99	8.39	8.79	9.19	9.59					
4882	-3.67	-3.27	-2.87	-2.47	-2.07	-1.67	-1.27	0.13	0.53	0.93	1.33	1.73	2.13	2.53	2.93	3.33	3.73	4.13	4.53	4.93	5.33	5.73	6.13	6.53	6.93	7.33	7.73	8.13	8.53	8.93	9.33					
4883	-3.93	-3.53	-3.13	-2.73	-2.33	-1.93	-1.53	0.39	0.79	1.19	1.59	1.99	2.39	2.79	3.19	3.59	3.99	4.39	4.79	5.19	5.59	5.99	6.39	6.79	7.19	7.59	7.99	8.39	8.79	9.19	9.59					
4884	-4.19	-3																																		

NOTES: Zonal Mean, Positive for Wind Component from West; Meridional Mean, Positive for Wind Component from South. Underlined Values Indicate Intraseasonal Correlations

TABLE #4: COVARIANCE OF RESULTANT WIND VELOCITY AT INDICATED ALTITUDES AT PATRICK AFB FOR THE WINTER MONTHS (meters/sec) <sup>2</sup>														COVARIANCE MATRIX	
STATION	STATION ELEVATION	STATION COORDINATES	PERIOD OF OBSERVATION	DATA SOURCE	PREPARED BY										PATRICK AFB, FLORIDA
Patrick AFB, Florida	7 meters MSL	28 deg 14 min N, 80 deg 16 min W	Feb 1950 - Feb 1955	R. E. Bieber's Report LMD 49703	Army Ballistics Missile Agency Aeroballistics Laboratory Redstone Arsenal, Alabama 16 May 1960										WINTER MONTHS
REFERENCE PERIOD Winter Months (Dec., Jan., Feb.)	Alt. (MSL) km	2	4	6	8	10	12	14	16	18	20	22	24	26	
sfc	26.43	28.92	28.04	29.46	30.59	32.88	23.94	11.10	9.59	7.15	3.28	0.40	0.79	1.53	
2		95.85	83.09	89.96	98.97	101.52	87.91	72.32	57.71	33.08	9.58	3.30	17.93	19.38	
4			180.28	140.14	155.59	165.13	145.45	124.65	97.07	61.54	24.35	13.50	21.37	31.84	
6				268.75	228.63	244.58	243.36	184.41	139.56	90.28	34.01	21.34	21.05	40.93	
8					424.57	352.52	320.77	259.67	197.69	129.71	50.42	17.48	24.49	52.37	
10						683.25	433.45	340.62	236.10	155.91	57.65	46.32	37.49	60.38	
12							783.90	407.03	285.80	179.81	60.49	40.15	31.32	55.39	
14								608.63	281.27	179.17	59.41	25.01	29.53	35.42	
16									376.23	163.92	80.21	47.80	38.75	38.67	
18										260.21	80.28	37.89	44.24	49.25	
20											162.06	60.14	57.94	63.62	
22												143.89	79.92	77.67	
24													188.98	117.37	
26														193.37	
Alt. (MSL) km	sfc	2	4	6	8	10	12	14	16	18	20	22	24	26	

TABLE #5: COVARIANCE OF RESULTANT WIND VELOCITY AT INDICATED ALTITUDES AT PATRICK AFB FOR THE MONTH OF JANUARY (meters/sec) <sup>2</sup>														COVARIANCE MATRIX	
STATION	STATION ELEVATION	STATION COORDINATES	PERIOD OF OBSERVATION	DATA SOURCE				PREPARED BY						PATRICK AFB, FLORIDA	
Patrick AFB, Florida	7 meters MSL	28 deg 14 min N, 80 deg 36 min W	Jan 1951 - Dec 1957	National Weather Records Center U. S. Weather Bureau Asheville, North Carolina				Army Ballistics Missile Agency Aeroballistics Laboratory Redstone Arsenal, Alabama 16 May 1960						JANUARY	
Alt. (MSL) km	Alt. (MSL) km	2	4	6	8	10	12	14	16	18	20	22	24	26	
sfc	sfc	28.97	28.63	30.21	30.16	29.02	20.58	15.39	6.09	9.68	3.13	4.67	5.85	5.82	
23.60															
2		98.61	96.79	104.74	104.51	104.15	87.55	64.42	39.43	16.93	2.84	7.99	7.88	2.01	
4		149.41	138.87	167.98	174.74	138.07	120.28	77.43	36.97	13.38	2.17	2.15	5.53		
6			283.98	245.45	253.15	231.72	178.30	104.16	49.05	16.52	1.28	7.92	6.14		
8				403.99	382.64	316.14	248.09	137.57	63.91	18.41	1.92	4.91	15.90		
10					683.68	427.49	314.09	170.05	83.93	35.34	5.22	2.82	10.04		
12						745.25	354.84	213.38	101.59	39.10	7.90	5.38	3.35		
14							508.81	193.73	92.74	47.18	17.50	0.19	13.41		
16								283.17	94.51	55.04	33.95	20.28	14.20		
18									143.84	43.55	33.31	28.49	29.48		
20										89.92	46.23	33.66	39.85		
22											94.65	59.64	48.36		
24												109.31	70.22		
26													133.62		
Alt. (MSL) km	sfc	2	4	6	8	10	12	14	16	18	20	22	24	26	

TABLE #6: COVARIANCE OF RESULTANT WIND VELOCITY AT INDICATED ALTITUDES AT PATRICK AFB FOR THE ANNUAL (meters/sec) <sup>2</sup>													COVARIANCE MATRIX		
STATION	STATION ELEVATION	STATION COORDINATES		PERIOD OF OBSERVATION	DATA SOURCE				PREPARED BY				PATRICK AFB, FLORIDA		
Patrick AFB, Florida	7 meters MSL	28 deg 14 min N, 80 deg 36 min W		Jan 1951 - Dec 1957	National Weather Records Center U. S. Weather Bureau Asheville, North Carolina				Army Ballistics Missile Agency Aeroballistics Laboratory Redstone Arsenal, Alabama 16 May 1960						
REFERENCE PERIOD															ANNUAL
Annual															
Alt. (MSL) km	Alt. (MSL) km	2	4	6	8	10	12	14	16	18	20	22	24	26	
sfc	sfc	24.49	22.98	22.88	22.08	20.89	18.70	12.30	10.11	7.27	3.97	3.06	4.78	6.49	
2	2	81.18	69.74	78.91	80.36	85.67	82.56	70.68	83.09	58.78	18.28	14.69	16.88	21.31	
4	4		124.49	127.45	143.13	163.27	167.26	147.18	110.39	75.10	43.66	36.33	42.02	52.08	
6	6			218.21	215.75	249.45	262.77	232.38	169.87	113.98	69.84	62.22	78.07	88.88	
8	8				342.33	381.29	371.26	323.60	232.31	155.39	96.97	87.38	96.95	122.44	
10	10					577.35	510.69	433.28	299.68	200.36	128.89	114.76	124.32	187.90	
12	12						753.78	526.96	361.15	236.29	148.42	138.80	148.88	182.40	
14	14							647.82	386.92	236.49	183.71	137.68	190.89	187.46	
16	16								362.53	201.51	134.13	117.69	126.97	188.89	
18	18									194.85	108.82	94.19	103.40	124.62	
20	20										114.14	83.80	89.83	104.93	
22	22											109.08	98.96	111.69	
24	24												137.54	138.53	
26	26													189.45	
Alt. (MSL) km	Alt. (MSL) km	2	4	6	8	10	12	14	16	18	20	22	24	26	



TABLE #7: COMPARISON OF TABLE #1 WITH TABLE #2 \*

TABLE #7: COMPARISON OF TABLE #1 WITH TABLE #2 .																					
STATION	STATION ELEVATION		STATION COORDINATES		* The values shown in Table 2 were subtracted from the values shown in Table 1											PREPARED BY				PATRICK AFB, FLORIDA	
Patrick AFB, Florida	7 meters MSL		28 deg 14 min N, 80 deg 36 min W													Army Ballistics Missile Agency Aeroballistics Laboratory Redstone Arsenal, Alabama 16 May 1960					
Altitude (MSL) km					sfc	2	4	6	8	10	12	14	16	18	20	22	24	26			
Altitude (MSL) km	Zonal Mean SD m/s	Meridional Mean SD m/s																			
			1.381	-0.808	-0.804	-0.058	0.811	1.309	1.723	1.343	0.790	0.570	0.331	-0.294	-0.278	-0.548					
			0.234	-0.413	-0.524	-0.264	0.055	0.406	1.430	2.280	1.777	0.853	0.970	0.205	0.829	0.045					
sfc	-0.606	0.105	0.019	0.011	0.007	0.031	0.004	0.067	0.108	0.113	0.173	0.167	0.087	0.120	0.022	-0.106					
2	-0.209	-0.299	-0.007	0.069	-0.055	-0.058	-0.046	0.024	0.060	0.045	0.043	0.088	-0.074	0.026	0.035	-0.241					
4	-0.108	-0.334	-0.020	-0.028	0.079	-0.022	-0.035	0.017	0.095	0.040	0.068	0.118	0.008	0.090	-0.020	-0.122					
6	0.380	-0.539	-0.053	-0.027	-0.040	0.024	-0.042	0.022	0.105	0.093	0.092	0.163	-0.006	0.029	-0.142	-0.113					
8	1.057	-0.162	-0.018	0.039	-0.001	-0.010	0.070	0.057	0.078	0.045	0.141	0.181	0.127	-0.007	-0.138	-0.045					
10	2.414	-0.306	-0.022	-0.001	-0.025	-0.017	-0.047	-0.008	0.022	0.033	0.114	0.118	0.031	0.043	-0.204	-0.003					
12	3.853	0.182	-0.074	-0.040	-0.121	-0.103	-0.099	-0.067	-0.056	-0.041	0.078	0.081	0.023	-0.027	-0.145	0.047					
14	3.813	1.652	-0.054	-0.029	-0.071	-0.101	-0.116	-0.090	-0.074	-0.121	0.060	0.117	-0.024	-0.062	-0.128	0.040					
16	2.547	2.541	0.019	0.099	0.013	0.035	0.064	0.045	-0.003	0.014	-0.138	0.018	-0.025	-0.123	-0.238	-0.130					
18	2.997	4.334	0.113	0.077	0.073	0.117	0.161	0.148	0.126	0.117	0.062	-0.023	-0.076	-0.121	-0.243	-0.113					
20	-0.452	3.133	0.123	0.119	0.106	0.117	0.123	0.046	0.021	-0.061	-0.065	0.004	-0.044	-0.084	-0.174	-0.149					
22	0.328	2.391	0.107	0.159	0.158	0.187	0.139	0.209	0.163	0.025	0.019	-0.106	-0.180	-0.018	-0.326	-0.127					
24	1.669	3.555	0.167	0.319	0.247	0.308	0.263	0.294	0.244	0.193	0.098	-0.008	-0.023	-0.076	-0.082	-0.164					
26	2.076	3.646	0.265	0.318	0.315	0.319	0.230	0.250	0.252	0.060	0.140	-0.014	0.015	0.023	-0.065	-0.213					

TABLE #8: COMPARISON OF TABLE #1 WITH TABLE #3 *																
STATION	STATION ELEVATION	STATION COORDINATES				*The values shown in Table 3 were subtracted from the values shown in Table 1				PREPARED BY				PATRICK AFB, FLORIDA		
Patrick AFB, Florida	7 meters MSL	28 deg 14 min N, 80 deg 36 min W								Army Ballistics Missile Agency Aeroballistics Laboratory Redstone Arsenal, Alabama 16 May 1960						
Altitude (MSL) km		efc	2	4	6	8	10	12	14	16	18	20	22	24	26	
Altitude (MSL) km	Meridional Mean m/s	0.811	-1.628	-1.184	-0.538	0.171	0.729	1.403	2.113	1.360	0.610	0.161	0.106	0.190	0.248	
	Zonal Mean SD m/s	0.414	1.387	1.666	2.666	3.305	3.826	3.220	2.640	2.987	2.103	1.090	-0.028	1.199	1.438	
efc	0.994	-0.085														
2	3.011	0.341														
4	5.822	-0.234														
6	8.830	-0.889														
8	11.907	-1.272														
10	15.144	-2.336														
12	17.303	-3.698														
14	17.613	-3.618														
16	15.527	-2.379														
18	12.767	0.574														
20	8.628	0.933														
22	9.018	1.371														
24	11.269	-0.965														
26	13.656	-0.444														

TABLE #9: COMPARISON OF TABLE #4 WITH TABLE #5 \*

TABLE #9: COMPARISON OF TABLE #4 WITH TABLE #5 *															
STATION Patrick AFB, Florida	STATION ELEVATION 7 meters MSL		STATION COORDINATES 28 deg 14 min N, 80 deg 36 min W		* The values shown in Table 5 were subtracted from the values shown in Table 4		PREPARED BY Army Ballistics Missile Agency Aeroballistics Laboratory Redstone Arsenal, Alabama 16 May 1960							PATRICK AFB, FLORIDA	
	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	
sfc	sfc	2	4	6	8	10	12	14	16	18	20	22	24	26	
2	2.83	- 0.05	- 0.59	- 0.76	0.96	3.86	3.39	- 4.30	-28.36	12.83	5.41	4.27	5.06	7.33	
4		- 2.76	-13.70	-14.79	- 5.54	- 2.63	0.36	5.89	18.29	16.15	6.74	11.29	25.51	17.34	
6		0.87	-18.74	-12.38	- 9.61	-12.62	4.37	19.64	24.57	24.57	12.97	15.47	23.69	24.31	
8			-15.23	-16.82	- 8.57	11.64	6.11	33.40	41.23	41.23	17.48	22.62	28.97	34.79	
10				20.58	- 0.12	4.63	13.72	60.12	65.80	65.80	32.01	19.40	31.40	36.47	
12					- 0.43	5.96	26.53	66.05	71.98	71.98	22.31	41.10	40.31	50.34	
14						38.65	66.09	70.42	78.22	78.22	21.43	32.24	36.70	58.72	
16							99.82	94.91	86.43	86.43	12.23	7.52	29.72	22.01	
18								93.06	71.41	71.41	25.17	13.85	15.48	24.47	
20									116.67	116.67	36.73	4.58	15.75	19.80	
22											72.14	13.91	24.28	45.19	
24												49.24	20.28	29.31	
26													79.67	47.15	
Alt. (MSL) km	sfc	2	4	6	8	10	12	14	16	18	20	22	24	26	

TABLE 80: COMPARISON OF TABLE 64 WITH TABLE 66 *													
STATION	STATION ELEVATION	STATION COORDINATES		*The values shown in Table 6 were subtracted from the values shown in Table 4		PREPARED BY Army Ballistics Missile Agency Aeroballistics Laboratory Redstone Arsenal, Alabama 16 May 1960							
Patrick AFB, Florida	7 meters MSL	28 deg 14 min N, 80 deg 36 min W											
Alt. (MSL) Alt. (MSL) km	Alt. (MSL) Alt. (MSL) km	Alt. (MSL) Alt. (MSL) km	Alt. (MSL) Alt. (MSL) km	Alt. (MSL) Alt. (MSL) km	Alt. (MSL) Alt. (MSL) km	Alt. (MSL) Alt. (MSL) km	Alt. (MSL) Alt. (MSL) km	Alt. (MSL) Alt. (MSL) km	Alt. (MSL) Alt. (MSL) km	Alt. (MSL) Alt. (MSL) km	Alt. (MSL) Alt. (MSL) km	Alt. (MSL) Alt. (MSL) km	Alt. (MSL) Alt. (MSL) km
2	2	4	6	8	10	12	14	16	18	20	22	24	26
2	2	4	6	8	10	12	14	16	18	20	22	24	26
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Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km	Alt. (MSL) km

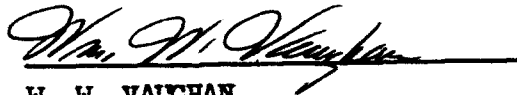
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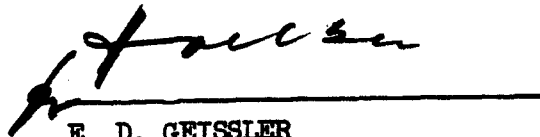
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